

Adsorption of Nickel Ions From Aqueous Solution Using Natural Clay

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Abstract

The adsorption characteristics of Nickel (II) onto Iraqi Bentonite clay from aqueous solution have been investigated with respect to changes in pH of solution, adsorbent dosage, contact time and temperature of the solution. The maximum removal efficiency of Nickel (II) ions is 96% at pH=6.5 and exposure to 100 g/L adsorbent. For the adsorption of Nickel (II) ions, the Freundlich isotherm model fitted the equilibrium data better than the Langmuir isotherm model. Experimental data are also evaluated in terms of kinetic characteristics of adsorption and it was found that the adsorption process for Ni²⁺ ions follows well pseudo-second-order kinetics. Thermodynamic functions, the change of free energy (ΔG°), enthalpy (ΔH°) and entropy (ΔS°) of adsorption are also calculated for Nickel (II) ions. The results show that the adsorption of the Nickel (II) ions on Iraqi Bentonite is feasible and exothermic at (20-50) °C.

Keywords: Adsorption, Nickel (II), Iraqi bentonite clay, Kinetics.

1 Introduction

The progressive increase of industrial technology results in a continuous increase of pollution, and a great effort has been devoted to minimize these hazardous pollutants, therefore, avoiding their dangerous effects on animals, plants and humans. Metals can pose health hazards if their concentrations exceed allowable limits. Even when the concentrations of metals do not exceed these limits, there is still a potential for long term contamination, since heavy metals are known to be accumulative within biological systems [1, 2]. Chromium, Nickel, Mercury, Copper, Zinc and Cadmium are frequently detect in industrial wastewaters, which are originate from pesticides, mining activities, battery manufacture, smelting, nuclear industry, metal plating, etc. Over the years some methods have been applied to remove the ions of metal from industrial wastewater and soils. The general traditional methods used for the removal of heavy metal ions from aqueous solutions include:

solvent extraction, phyto-extraction, ion-exchange chemical precipitation, and ultra-filtration, reverse osmosis, electro dialysis and adsorption.

Adsorption with low-cost adsorbents has been effectively applied to eliminate heavy metals from contamination solutions [3]. Nickel is a main worry due to its normal use in developing countries with its non-degradable nature. The Nickel persistent toxicity to the environment and humans is also familiar and high Nickel concentrations cause gastrointestinal annoyance, cancers of bone and lung. In recent years, different adsorbents have been used for elimination of Nickel (II) from contaminated solutions [4, 5]. On the other hand, novel adsorbents by local availability, great adsorption capability and economical composed materials are still desirable.

The bentonite clay can be found in many types are following the individual main element; such as calcium (Ca), aluminum (Al), Sodium (Na) and potassium (K). Experts discuss a nomenclatorial problems number in the bentonite clays classification. Usually bentonite forms from the volcanic ash weathering, mainly frequently in the presence of water. Bentonite has been widely used as a foundry-sand bond in iron and steel foundries. Bentonites are usually used for decolorizing various mineral, vegetable, and animal oils [6,7]. Bentonite has in adsorbing property and relatively great amounts of protein molecules from contamination solutions. Bentonite is used in a diversity of favorite care things for example it can be used in cat trash to take up the feces contain and odor. It is also used to take up grease and oils.

The objective of the present study is to investigate the adsorption potential of Iraqi Bentonite clay in the removal of Ni²⁺ ions from aqueous solution. The effects of pH, adsorbent amount, contact time and concentration of metal ions in the solution. The Freundlich and the Langmuir isotherms models are used to explore the equilibrium statistics. In addition, the Nickel(II) ions adsorption mechanisms on the clay are also evaluated within thermodynamics and kinetics conditions.

2 Materials and procedure

2.1 The Preparation of adsorbent

From the Geological Survey and Mining Company (Iraq/ Baghdad) were obtain Iraqi bentonite samples. The Iraqi bentonite samples, which were obtained, used with no chemical treatment. The Iraqi bentonite chemical compositions are determined by the X-Ray as shown in Table (1).

Table 1: Chemical composition of I Bentonite Clay (%).

Compound	Mass (%)	Compound	Mass (%)
SiO ₂	56.9	CaO	1.5
Al ₂ O ₃	25.0	Na ₂ O	1.5
Fe ₂ O ₃	8.9	MgO	1.2
TiO ₂	1.6	K ₂ O	1.0

The Iraqi bentonite clay specific surface area is 2.2 m²/gm. (Table 2).The particle size ranged between 25 and 50 μm and its porosity was 75%. Similarly, reported BET surface areas of 1.083 m²/g and 2.52 m²/g for activated carbon from macadamia nuts used for phenol removal and maize tassels for heavy metal removal from polluted waters, respectively although adsorbents with higher surface areas have been widely reported in literature.

Table 2: Characteristics of Iraqi Bentonite Clay

Physical Parameters	Result
BET surface area (m ² /gm)	2.2
Micropore surface area (m ² /g)	1.25
Total pore volume (cm ³ /g)	0.02
Micropore volume (cm ³ /g)	0.001
Average pore diameter(Ao or 10 ⁻⁸ cm)	250

2.2 Adsorbate solution

Nickel solution was prepared by using the Nickel sulfate (NiSO₄.6H₂O) in an analytical mark. The solution of Ni⁺² ions was prepared to containing 1000 mg/l of Ni⁺² ions. In the study all solutions prepared by double distilled water.

2.3 Adsorption Study

Experiment of adsorption was follow up at the adsorbent dosage level, contact time , and value of desired pH by the required adsorbent in 500ml conical flasks containing solutions of Nickel(II) ions in(100 ml). Initial concentrations of metal were (25, 50and 75) mg/l. Samples were collected at (10, 20, 30, 50, 70, 90, 120 and 140) min to decide the optimal time of shaking. The adjusted values of pH were (2, 3, 4, 5, 5.5, 6, 6.5, 7, and 8) by using 0.1M H₂SO₄ or 0.1M NaOH solution. The adsorbent dosage effect on Nickel(II) removal was studied by using various Ni⁺² concentrations in conjunction with (10, 20, 40, 60, 80, 100,150,180 and 200) g/L of Iraqi bentonite. The studies of adsorption were also

follow up to find out the temperature effect at (20, 30, 40, and 50)°C and to evaluate the thermodynamic parameters of adsorption. Throughout the process of adsorption, flasks were shacked at 200 rpm on a shaker. The flasks content were filtrated throughout filter paper and filtrate was analyzed for the concentration of metal by the Atomic Absorption Spectrometer [AAS]. The amount of Ni⁺² absorbed per unit mass of adsorbent (qe) was calculated by the following equation.

$$q_e = \frac{(C_i - C_e)V}{m} \dots\dots\dots (1)$$

where C_i and C_e represent the initial and equilibrium concentrations of metal ions in aqueous phase. V is the volume of the solution in liters (l) and M is the mass of the adsorbent in grams. The metal ions adsorption percentage was calculated by the equation :

$$\text{Adsorption}(\%) = \frac{[C_i - C_f]}{C_i} \times 100 \dots\dots\dots (2)$$

where C_i and C_f are the initial and final metal ion concentrations, respectively. The average absolute value of relative error (AARE) was used to contrast the experimental data with predicted results. That is defined as follows:

$$AARE = \frac{1}{NDP}$$

$$\sum_{i=1}^{NDP} \frac{|\text{Predicted value} - \text{Experimental value}|}{\text{Experimental value}}$$

in which NDP is the number of data point [8] .

3 Result and Discussion

3.1 Adsorbent Dosage Effect

In adsorption processes, Adsorbent dosage is one of the important parameters because, it's determine the adsorbent capacity for a given adsorbate initial concentration below a given operating conditions set. Figure (1) shows the adsorbent dosage effect on the Nickel(II) ions adsorption. From the figure, it could be noted that there is an increases in the percentage of adsorption when adsorbent dosage increases starting, from 25 to 96% for Ni⁺² ions. The increases of removal efficiency may be attributed to the truth that, an adsorbent dosage increases, a new surface of adsorbent would be available to adsorb the solute [9].

3.2 pH Effects

pH is one of significant parameters that lead to metal ions sorption on different adsorbents is the adsorbate solutions. That is partly because of the nature of hydrogen ion itself as a strong competing sorbate and partially to the truth that the pH of solution can influence the chemical speciation of metal ions. The pH effects on nickel

ions adsorption onto Iraqi bentonite clay is shown in Fig.2. This figure show that at low values of pH, the adsorption efficiency is low; because of increasing in positive charge density(protons) on the clay surface sites, resulting in an electrostatic repulsion among the (Nickel(II) ions and edging groups with positive charge (Si-OH⁺₂) on the surface[10]. When the pH increases the electrostatic revulsion decreases due to the surface positive charge density is reduction on the sorption ends, therefore on the surface resulting increase in the adsorption of metal ion. Iraqi bentonite surface in an alkaline medium becomes negatively charged. Consistent with Figure (2), the metal ions maximum adsorption occur at pH 6.5. When values of (pH ≥ 7), the adsorbent capacity was decreased due to metal precipitation and metal ions accumulation. Thus, the best pH value was 6.5 and this pH value was selected for the next experiments.

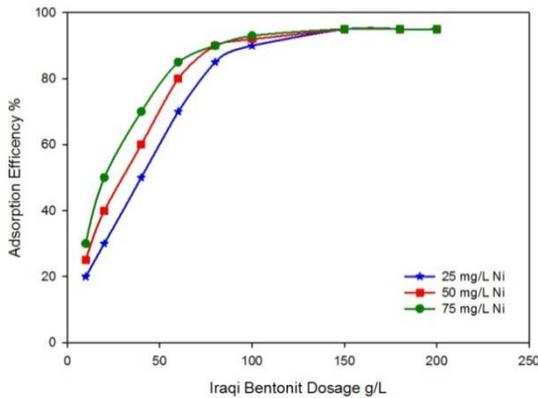


Figure 1: Iraqi Bentonite Dosage effects on the Ni²⁺ ions adsorption Efficiency in various concentration.

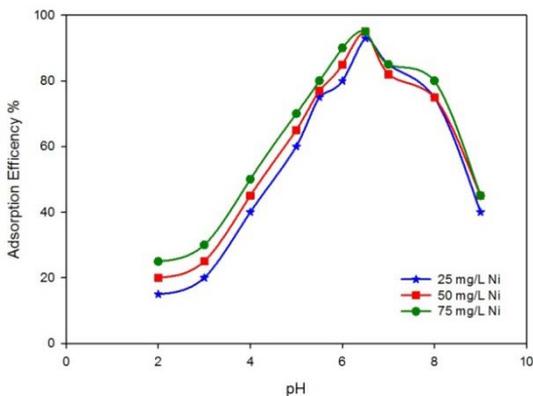


Figure 2: pH Effects on Ni²⁺ ions adsorption efficiency % on Iraqi bentonite various concentration.

3.3 Shaking Time Effects

Adsorption of Ni²⁺ ions on Iraqi bentonite clay in related in to the shaking time is illustrated in Figure (3). From this figure, notes the

concentration of Nickel (II) in aqueous solution has rapidly decreased through the first half hour and remained nearly stable after 90 min, signifying that the metal ions adsorption is quick. Thus, 90 min is selected as the optimum shaking time for Ni²⁺ ions removal.

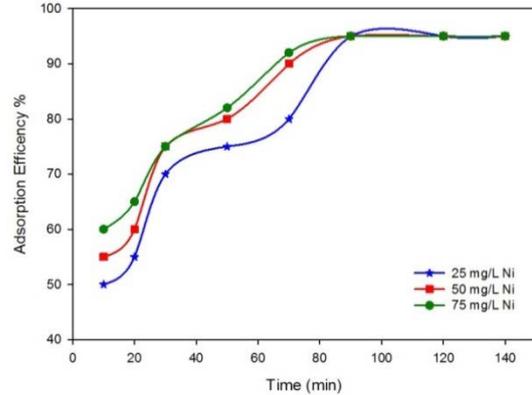


Figure 3: Contact time effect of Ni²⁺ ions adsorption efficiency % on Iraqi bentonite in various concentrations.

3.4 Isotherm Models of Adsorption

The equilibrium adsorption isotherm can be considered fundamental importance in the adsorption design systems. Langmuir Model is suitable for monolayer adsorption onto a surface containing a limited quantity of the same sites, this model is most frequently used to characterize data on solution adsorption. The adsorption isotherm exact shape for a heterogeneous adsorbent depends on the KL values distribution, and more particularly on the adsorbent regularity distribution of the site adsorption energies [11]. This model can be expressed as:

$$q_e = \frac{q_m KL C_e}{1 + KL C_e} \dots\dots\dots(3)$$

$$\text{or } \frac{C_e}{q_e} = \frac{1}{q_m KL} + \frac{C_e}{q_m}$$

where q_e is the equilibrium metal ion concentration on the adsorbent (mg/g), C_e the equilibrium metal ion concentration in the solution (mg/l), q_m the monolayer adsorption capacity of the adsorbent (mg/gm) and KL represents the Langmuir adsorption constant (l/mg), related to the free energy of adsorption. The adsorption type was valid when: (1) the surface of adsorbent is homogeneous; (2) both bulk and surface phases show ideal behavior; and (3) the film of adsorption is monomolecular.

The model of Freundlich [12] is an empirical equation and can be applied for non-ideal sorption on heterogeneous surfaces and multilayer sorption. The equation is commonly given by:

$$q_e = K_L (C_e)^{1/n} \dots\dots\dots(4)$$

where K_L is a constant related to the adsorption capacity and 1/n is an empirical parameter related

to the adsorption intensity, which varies with the heterogeneity of the material.

The Langmuir isotherm non-linearized form was used to get the model constants [13]. The Langmuir model constants are shown in Table (2). The coefficient of correlation (R^2) was found to be 0.953 for the Ni^{+2} ions adsorption representing that the model of Langmuir is capable to explain the metal ions adsorption adequately. The maximum capacity value (q_m) was found to be 2.24 (mg/g) for Ni^{+2} ions. The KL value is 1.922 (l/mg) for Ni^{+2} ions.

The isotherm shape can also be considered when predicting whether an adsorption system is "favorable" or "unfavorable". The Langmuir isotherm essential characteristic can be expressed in terms of a dimensionless separation factor or parameter of equilibrium (R) [13], which is defined by the following equation:

$$R = \frac{1}{1+KL C_e} \dots\dots\dots (5)$$

According to the value of R, the isotherm shape may be interpreted as described in Table (4). As shown in Table (3), the adsorption of Ni^{+2} ions onto Iraqi bentonite is favorable. A plot of $\ln q_e$ vs $\ln C_e$ enables the empirical constants KF and $1/n$ to be determined from the intercept and slope of the linear regression. From Freundlich isotherm obtained by Figure (5) shows plotting $\ln C_e$ vs. $\ln q_e$ values. For the isotherm of Freundlich model the results presents in Table (2) correlation coefficient and constants. For Ni^{+2} ions Kf values and $1/n$ are set up to be 1.22 and 0.20. Between 0 to 1 are found $1/n$ values, representing that the metal ions adsorption onto Iraqi Bentonite is good in the special operating conditions.

For Ni^{+2} ions the values of R^2 are found to be 0.9657. The experimental comparison data by q_e values obtain from both models are shown in Figures (4) and (5). From these figures, the results of adsorption data obtained are best described with the Freundlich isotherm model.

Table 3: Constants of Langmuir and Freundlich for Ni^{+2} ions adsorption on Iraqi Bentonite.

Langmuir model	q_m (mg/g)	KL (l/gm)	R	AARD%
	2.24	1.922	0.0169 -0.866	14.72
Freundlich model	$1/n$	Kf		AARD%
	0.2	1.22		6.42

Table 4: Separation factor for Shape of Isotherm

Value R	Type of Adsorption
$R > 1.0$	Unfavorable
$R = 1.0$	Linear
$0 < R < 1.0$	Favorable
$R = 0$	Irreversible

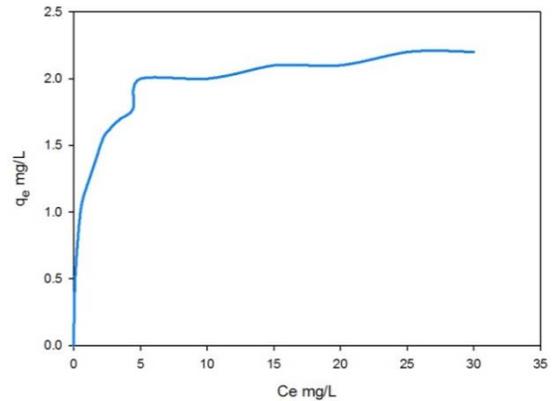


Figure 4: Experimental data of the q_e values for Ni^{+2} ions obtained by Langmuir isotherms.

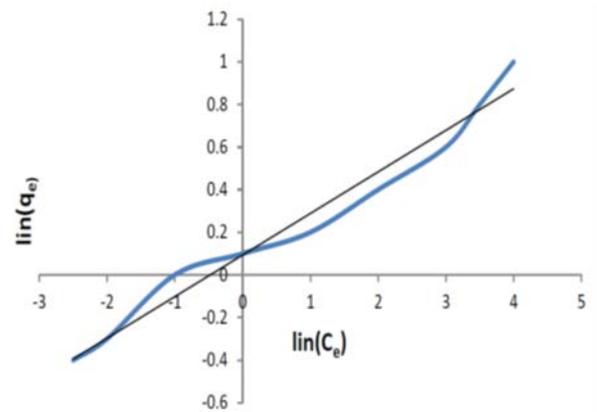


Figure 5: Experimental data of the q_e values for Ni^{+2} ions obtained by Freundlich isotherms.

3.5 Kinetics of Adsorption

In order to clarify the Ni^{+2} ions kinetics of adsorption on Iraqi bentonite Lagergren pseudo-first-order and pseudo-second-order kinetic models are applied to the experimental data. Many researchers have studied the heavy metals kinetics adsorption by using Lagergren pseudo-first-order rate equation [14] and as follows:

$$\ln(q_e - q_t) = \ln q_t - K_1 t \dots\dots\dots (6)$$

where q_t (mg/g) is the amount of the metal ion adsorbed at t (min) and k_1 is the constant rate of the adsorption (min^{-1}). Figure (6) show the Lagergren pseudo-first-order model for the Nickel ions kinetics adsorption on Iraqi Bentonite [15].

Study the heavy metals adsorption kinetics on peat used a pseudo-second-order reaction rate equation. This equation is known in:

$$\frac{t}{q_t} = \frac{1}{K_2 q_e^2} + \left\{ \frac{1}{q_e} \right\} t \dots\dots\dots (7)$$

where k_2 (g/mg min) is the constant rate of the pseudo-second-order equation. This model is more likely to predict the adsorption behavior kinetic by chemical sorption [16].

From this equation the calculated correlation coefficient and the rate constant (k_2) are listed in Table (5). It's clear from the results that the

Ni⁺² ions adsorption onto Iraqi Bentonite follows well the kinetics of the pseudo-second-order. Ho's pseudo-second-order model is show in Figure (7) for the Nickel (II) ions adsorption kinetics on Iraqi Bentonite.

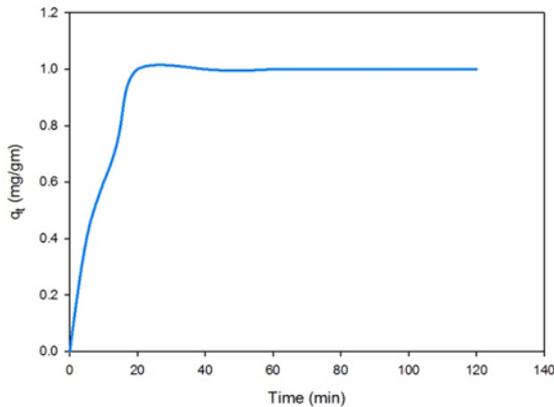


Figure 6: Adsorption of Ni⁺² ions on Iraqi Bentonite by The Lagergren Pseudo-first-order model.

The constants of first-order rate from this study with other studies comparison show that the rate of Nickel adsorption on Iraqi bentonite is relatively quick [17].

Table 5: Ni⁺² ions Adsorption on to Iraqi Bentonite by Lagergren rate equation constants and Pseudo-second-order rate constant.

Lagergren rate equation	K1 (1/min)	R ²	AARD %
	0.177	0.92	9.49
Pseudo-second-order rate equation	K2 (gm/mg.min)	R ²	AARD %
	0.193	0.991	7.60

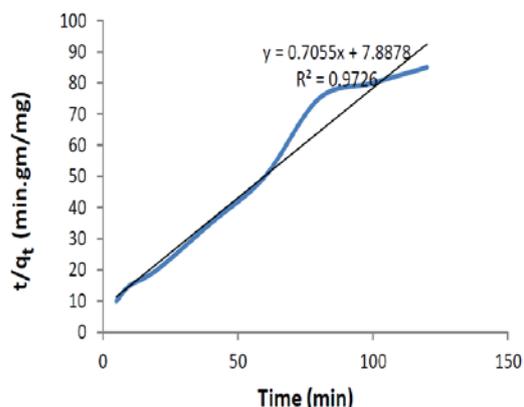


Figure 7: Adsorption of Ni⁺² ions on Iraqi Bentonite by model of Ho's Pseudo-Second-order.

3.6 Adsorption Thermodynamics

In this study, the range of temperature from (20 to 50) °C was used. The parameters of Thermodynamic, including the free energy

changes (ΔG°), the enthalpy changes (ΔH°) and entropy changes (ΔS°), were determined by the following equations [18]:

$$\Delta G^\circ = -RT \ln KD \dots\dots\dots (8)$$

$$\Delta G^\circ = \Delta H^\circ - T \Delta S^\circ \dots\dots\dots (9)$$

where R is the universal gas constant (8.314 J/mol.K), T is the temperature (K) and KD is the equilibrium constant. Enthalpy changes (ΔH°) and Entropy changes (ΔS°) of adsorption are obtained from equation below:

$$\ln KD = (\Delta S^\circ / R) - (\Delta H^\circ / RT) \dots\dots\dots (10)$$

Consistent with Eq. (10), the parameters (ΔH° and ΔS°) can be calculated from the intercept and slope a plot ($\ln KD$ vs. $1/T$), respectively (Figure 8).

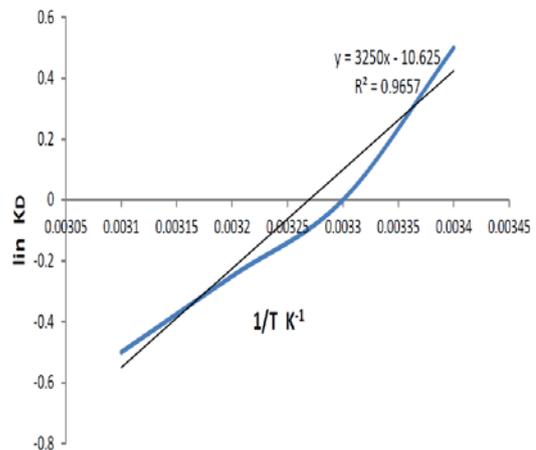


Figure 8: Thermodynamic Parameters for Ni⁺² ions Adsorption on Iraqi Bentonite.

To calculated the adsorption Gibbs free energy changes (ΔG°) from Eq. (8) by calculate $\ln KD$ values for various temperatures. ΔG° values are set up to be (-1.34, -0.3, 0.62 and 1.29) kJ/mol for Ni⁺² ions adsorption at (20, 30, 40 and 50) °C, respectively.

ΔG° negative values specify that thermodynamically feasible with the adsorption natural environment of Ni⁺² ions at (20 and 30) °C. ΔG° positive and small values specify that feasible but non-spontaneous process. The value of ΔH° parameter is (-26.48 kJ/mol) for the Ni⁺² ions adsorption, That means negative value is specify the Ni⁺² ions adsorption is of exothermic nature onto Iraqi Bentonite in the temperature range from 20°C to 50°C. The ΔS° values are set up to be (-6.31) J/mol. °K for the Ni⁺² ions adsorption. The ΔS° negative values suggest a reduce in the un-certainty at the solid/solution interface through the Ni⁺² ions adsorption on Iraqi Bentonite clay [19].

4 Conclusions

Nickel (II) ions adsorption behavior on Iraqi bentonite clay was investigated in a group of experiments. There are many parameters that can effect on the adsorption reaction. This was set up to be drastically dependent on adsorbent dosage, contact time, and pH. The Ni⁺² ions adsorption speed was rapid. The Nickel-Bentonite system reached to equilibrium within 90min. For Ni⁺² ions adsorption state optimum pH was found to be 6.5. From the data of isotherm analysis it appeared that Ni⁺² ions adsorption pattern on Iraqi Bentonite clay was followed the Freundlich model. The Iraqi Bentonite clay greatest capacity was predicted to be 2.24 (mg/g) for Ni⁺² ions, when the equation of Langmuir model is used. The Ni⁺² ions best kinetic data was described in the reaction rate of pseudo-second-order model. Thermodynamic parameters explain the adsorption and the process was favorable exothermic nature.

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استخدام الطين الطبيعي لامتنزاز أيونات النيكل من محلول مائي

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الخلاصة

تم التحقق من خصائص عملية امتزاز ايونات النيكل على البنتونايت العراقي من محلول مائي بدلالة التغيرات في الدالة الحامضية pH للمحلول المائي ، كمية المادة الممتزة، زمن التلامس ودرجة الحرارة للمحلول المائي . من خلال التجارب تم الحصول على اعلى كفاءة إزالة لأيونات النيكل بالامتزاز عند قيمة الدالة الحامضية 6,5 والمادة الممتزة 100 غرام / لتر تساوي 96% في عملية امتزاز ايونات النيكل تبين ان الامتنزاز حسب Freundlich isotherm model تكون النتائج متوازنة افضل مما لو كانت حسب Langmuir isotherm model. تم تقييم البيانات التجريبية أيضا من حيث الخصائص الحركية للامتزاز وتبين أن عملية امتزاز أيونات النيكل تتبع جيدا نظام حركية معادلة من الدرجة الثانية الزائفة. الوظائف الترموديناميكية ، التغير في الطاقة الحرة (ΔG^0)، المحتوى الحراري (ΔH^0) والانتروبي (ΔS^0) للامتزاز أيضا تم حسابها لايونات النيكل الثنائية. وأظهرت النتائج أن امتزاز أيونات النيكل الثنائية على البنتونايت العراقي ممكن ويكون التفاعل باعث للحرارة في 20-50 درجة مئوية